

INSPECTION REPORT

General Cargo International Terminal

JMT Project No: 18-02353

Submitted to: CLEVELAND - CUYAHOGA COUNTY PORT AUTHORITY



Photo by Port of Cleveland.com



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Executive Summary

This report summarizes the inspection and condition assessment of the waterfront infrastructure along the General Cargo Terminal from Dock 22 to Dock 28. Specifically, the inspection included the following infrastructure assets:

- 1) Sheet piling bulkheads
- 2) Piling caps
- 3) Fender systems
- 4) Timber curbing
- 5) Mooring bollards and connections
- 6) Outfall penetrations
- 7) Pavement adjacent to bulkheads

Additional items that were completed with this scope of work includes creation of a Maritime GIS database and webmap, hydrographic survey and construction repair details for bulkhead breaches. The inspection assessment condition of the infrastructure listed above is contained in the GIS webmap and can be accessed through ArcGIS credentials that have been provided to the Port Authority.

The age of the docks varies from the 50's, 60's and 90's and exhibit various signs of degradation over the relative time periods, but also some docks are used more frequently causing repair needs due to the volume of ships and landside cranes and vehicles loading and unloading payloads. The infrastructure that will require short- and long-term investments per dock is summarized below. Short-term repairs should be completed within a two-year time period and long-term improvements completed within a five-year time period.

Dock 22 – Constructed in 1998 is in good condition with minor repair items required.

Short Term Repairs: \$82,100 Long Term Improvements: \$95,200

Dock 24 – Constructed in 1965 is in adequate condition with minimal repairs given the age and volume of traffic.

Short Term Repairs: \$ 114,900 Long Term Improvements: \$ 1,285,900

Dock 26 – Constructed in 1958 is in marginal condition with a significant investment repair required due to multiple breach locations along the west bulkhead at the mudline elevation.

Short Term Repairs: \$ 118,400 Long Term Improvements: \$ 4,056,600

Dock 28 – Constructed in 1956 is in adequate condition given the age of the dock. There are several short term maintenance repairs that can extend the life expectancy of this bulkhead.

Short Term Repairs: \$ 66,500 Long Term Improvements: \$ 647,900



Inspection and Assessment

The above and below water inspection started on October 15, 2018 and was completed on February 17, 2019. The above water inspection consisted of a visual and hands-on inspection with GPS photography that has been incorporated into the GIS webmap. The inspection assessment consists of a numerical rating, as used by the Maryland Port Authority for the Port of Baltimore Facility, which is also displayed on the webmap by the specific asset layer. If an asset is rated a 1 (Poor Condition) the item requires complete replacement because it is missing or is no longer functioning per the original design intent. A rating of 2 means the asset requires repair within the short term maintenance plan of one to five years. An asset that is rated 3 shows sign of degradation and should be included in the longer term maintenance plan of five to ten years. A rating of 4 indicates that the item is currently in good condition but do to the nature of the asset it will more than likely require repair/replacement after ten years. If an asset is functioning as designed and it appears the material will last it's anticipated life cycle it is rated as a 5.

Good		Fair		Poor
5 Excellent	4 Good	3 Adequate	2 Marginal	1 Poor

The below water inspection consisted of a hands-on inspection with steel thickness measurements obtained on 25' intervals at the top of the water, mid-height and at the mudline. The 25' interval inspection was supplemented with an underwater sonar using a Sea Scan Arc Explorer towfish with a resolution of a ½" across the sonar scan. An example of the sonar scan output for Dock 26W is included below in Figure 9. Breaches and defects that were noticed in the output of the sonar scans on Dock 26 W and Dock 28 W were field verified by an underwater hands-on inspection. The steel thickness measurement readings are included in Appendix B.

A hydrographic survey of the lake bottom was also completed using Trimble sonar receiver and HYDROpro software to generate a contour map at 1' intervals that is colored coded and displayed in the webmap. The color codes correspond to the following water depths and an image of the contour model is included in Appendix A.

Blue:	30' – 25'
Green:	25' – 20'
Yellow:	20' - 10'
Orange:	10' – 5'
Dark Orange:	4' or less

In addition to the sonar readings, depth soundings were also collected at 25' intervals along the bulkhead and can be viewed on the webmap with the bulkhead thickness measurements. The survey data conforms to Ohio State Plane (Ohio North) Grid and 1985 vertical International Great Lakes Datum.





Findings

The infrastructure items that were inspected were also surveyed using Ohio State Plane Ground Coordinates and assigned an inspection code rating. This enabled the data to be uploaded to the GIS webmap with the correct coordinate location and condition rating. Per the example below, each mooring bollard was surveyed with a specific survey point identification number and color coding, which corresponds to the legend in the GIS webmap and the assessment chart above. When an item is reinspected, the assessment code can be directly edited in the GIS webmap in the field via laptop or tablet. After any repair or construction project, the GIS webmap should be updated with new survey and code rating information.

The findings of the inspection are described below per dock with a summary table of deficiencies for each asset. The inspection assessment and deficiencies can also be viewed in the GIS webmap as shown below with the mooring bollard layer turned on.



DOCK 22

Dock 22 was constructed in 1998 in close conformance to the original construction plans. In lieu of a 45degree bend in the northwest corner of the bulkhead, it was constructed as a perpendicular corner providing more area at the north end of the dock. Also, the bulkhead was constructed using the AZ-48



sheet piling (73' max. length) instead of the ZH-9.5 sheeting section with the series of HZ-775A piles. Overall, the sheet piling, fender system, mooring bollards and steel pile cap are in good condition. There are minor repairs required on the pile cap, timber curbing and fender system and moderate pavement replacement areas. Quantities for each asset that require repair or replacement are summarized in the table below.

Table 1 – Dock 22 Asset Deficiencies						
Asset	Deficiency	Quantity				
Fender system	Connection failure	2 each				
Fender system	Damaged	12 ft				
Pavement	Settled and damaged	180 sf				
Timber curbing	Missing	30 ft				
Pile cap	Damaged	20 ft				
Fire hydrant bollard	Damaged/bent	2 each				



Fig. 1 - Pavement settled and damaged (drainage outlet)



Fig. 2 – Break in timber curbing



Fig. 3 – Damaged pile cap



Fig. 4 – Damaged fender (1) and failed connection (2)



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DOCK 24

It appears that Dock 24 was constructed per the 1965 construction plans. The sheet piling used for the dock was a mixture of reinforced and unreinforced MZ38 at 80' and 70' lengths respectively. The unreinforced sheets were used at the south headwalls and reinforced sheets for the dock. The difference in material types of a reinforced and unreinforced sheeting section is a higher yield strength of 50 ksi versus 36 ksi, which saved steel weight for an increase in section modulus. Steel thickness measurements obtained on Dock 24 exhibit minimal section loss.

Along the south headwall between Docks 24 and 26, there is a 24" outfall with corrugated metal pipe (CMP) that has deteriorated behind the bulkhead causing loss of backfill material and pavement as shown below.



Fig. 5 – Sinkhole at CMP Outfall



Fig. 6 – Section loss at outfall (underwater)

The Port will be completing repairs on the outfall shown in Figures 5 and 6 under a 2019 repair contract.

The dock is in adequate condition given the high traffic and live load conditions that are subjected to the infrastructure. Short term repairs are needed on the timber curbing, fender system and mooring bollard/cleat foundations. Long term repairs are required on the cast in place concrete pile cap. Quantities for each asset that require repair or replacement are summarized in the table below.

Table 2 – Dock 24 Asset Deficiencies							
Asset	Deficiency	Quantity					
Mooring bollard/cleat	Deteriorated foundation	5 each					
Mooring bollard	Corroded anchor bolts	2 each					
Fender system	Missing/not functioning as designed	400 ft					
Timber curbing	Missing	15 ft					
Pile cap	Damaged	1100 ft					
Fire hydrant bollard	Damaged/bent	1 each					





Fig. 8 – Deteriorated pile cap and break in timber curbing

Fig. 7 – Deteriorated pile cap



Fig. 9 - Deteriorated mooring cleat foundation



Fig. 10 - Corroded anchor bolts

DOCK 26

Dock 26 was formerly called the West 6th Street Pier and it appears that it was constructed in 1958 over a river confluence to Lake Erie per the original construction drawings. The sheet piling used for the dock is a mixture of reinforced and unreinforced MZ38 at 70' and 60' lengths respectively. The reinforced sheets are strengthened with 6"x 7/8" Plate, 25' in length starting 18' below the top of the piling. Per the original plans, the reinforced sheets were primarily used along the west dock face and approximately 222' on the south corner of the east dock. For the sheet piling that was inspected on the east dock that contained the plates, most of the steel thickness measurements were taken adjacent to





the plate so that the sheeting thickness could be obtained. Steel thickness measurements obtained on Dock 26 East exhibit minimal section loss. However, there are numerous locations of section loss along the mudline on Dock 26 West that were identified in the sonar scan (image below) and field confirmed in four locations.



Fig. 11 – Holes along mudline of Dock 26 West

There are approximately 58 locations over 550' of bulkhead on the west dock that are similar to the holes in Figure 11. Most of the holes are along the mudline and there are a few that are close to midheight of the exposed sheeting. The first area of section loss was noticed 130' from the south end of the dock. From that point to the north end of the dock they are sporadically located with a high concentration around the mid-length of the dock and the north end, 400' and 590' from the south headwall respectively. The average hole size is $1.5' \times 1.0'$. Within this area, there was a repair project completed in 1999 to strengthen a section of wall, approximately 40' in length that was deflected outward at the mudline. The fact that the deflection was at the mudline indicates that the failure is at or below the mudline opposed to a top surcharge load or tieback failure. Below is a plan view detail of the repair, note the mention of "punctures, rips and tears" in the sheeting.





Given the quantity of breaches along the west dock, the bulkhead is in poor condition. On average, the dock as an infrastructure asset is in marginal condition. There are a high number of repairs required currently on the fender system and timber curbing, however these items might be replaced with the replacement of the existing bulkhead. Quantities for each asset that require repair or replacement are summarized in the table below.

Table 3 – Dock 26 Asset Deficiencies							
Asset	Quantity						
Sheet piling	Section Loss	550 ft					
Mooring bollard/cleat	Deteriorated foundation	3 each					
Fender system	Missing/not functioning as	1200 ft					
	designed						
Timber curbing	Missing	40 ft					
Timber curbing Damaged		120 ft					
Pavement/Drainage repair	Damaged/settled	80 sf					



Fig. 13 - Damaged fender system



Fig. 14 – Break in timber curbing



Fig. 15 – Damaged timber curbing and settled pavement



Fig. 16 - Sink hole behind south headwall



DOCK 28

Dock 28 was constructed in 1956 and was designed by the same company that designed Dock 26, therefore there are similar details that were used for both docks. The bulkhead for Dock 28 is constructed with the same sheet piling as Dock 26, MZ38, however it was not reinforced with steel plates or higher yield stress material. The sheet piling length is 60' and it is tied back to a deadman system 80' behind the wall.

The tieback system is a critical component for the wall stability, therefore it was exposed behind the bulkhead to inspect and verify the existing condition. Based upon available records, this is the first inspection to uncover the tieback system for evaluation. The condition of the steel tieback, waler and concrete deadman was in very good condition with little to no section loss observed. The elevation of the tieback system is approximately 1'-2' below the groundwater elevation (at the date of exposure, January 2019). Below are photographs of the exposed tieback and top portion of the tiebacks until either a repair of the bulkhead is required or the system is still in use in 10 years, 2029.



Fig. 17 – Tieback and Deadman Exposure



Fig. 18 - Tieback and Waler Exposure

Steel thickness measurements obtained on Dock 28 exhibit minimal section loss. However, there is one relatively large breach in the bulkhead 80' south of the north corner. The size of the breach is approximately 10' x 2' at the maximum ellipsoid shape of the opening (see Figure 20 below) and there is a sinkhole behind the bulkhead in this location that is approximately 80 sf. A repair was made behind the breach by installing a line of sheet piling, however the ends of the sheet piling run were not closed or sealed. The open ends allow backfill to escape and creates a void behind the wall and depression in the asphalt pavement. The Port will be backfilling this area as needed. Additionally, the walls of



Fig. 19 – Section Loss in CMP Outfall



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the 12" CMP outfall at the North end of the dock has deteriorated much like the outfall between Docks 24 and 26.

The dock is in fair condition given the age of the infrastructure, the breach in the bulkhead and the needed repairs on the fender system. The mooring bollards are in good condition and the timber curbing is aged, but a majority of the curbing is functioning as designed. Quantities for each asset that require repair or replacement are summarized in the table below.



Fig. 20 – Breach in Dock 28

Table 4 – Dock 28 Asset Deficiencies							
Asset	Deficiency	Quantity					
Sheet piling	Breach	25 ft					
Mooring bollard	Broken ear cleat	1 each					
Fender system	Missing/not functioning as designed	180 ft					
Fender system	Damaged	640 ft					
Timber curbing	Damaged	110 ft					
Pavement and backfill	Damaged	80 sf					



Recommendations

The recommended repairs are based on maintaining the docks in their current role and function, and information garnered from review of the existing plans, inspection observations and engineering judgement. The anticipated remaining useful life is based on the life design expectancy of the infrastructure item and subtracting the age of that item. The basis of the life design expectancy that has been set for the sheet piling bulkhead is 70 years. The life design expectancy of an item can vary depending on maintenance, frequency of use and the environmental surroundings. All of these factors could decrease or increase the life expectancy of an infrastructure asset, is an important step to take when evaluating safety, costs and budgets for repair versus replacement.

The estimated construction costs for the recommended repairs below include design, construction, construction inspection and a contingency cost of 20%. It is anticipated that the short term repair items would be funded through an annual maintenance budget and the larger financial and long term items would need to be included in future capital investment budgets.

Dock 22

Anticipated Remaining Useful Life: 40 years Preventative Maintenance Plan: Timber Curbing = \$ 12,600 Pavement Repairs = \$ 26,400 Pile Cap Repairs = \$ 33,700 Bollard Repairs = \$ 9,400 Capital Investments: Fender System Repairs = \$ 95,200 Inspection Frequency: 5 years

Dock 24

Anticipated Remaining Useful Life: 10 years Preventative Maintenance Plan: Timber Curbing Repairs = \$ 14,400 Mooring Bollard Repairs = \$ 100,500 Capital Investments: Concrete Pile Cap Repairs = \$ 1,087,100 Fender System Repairs = \$ 198,800 Inspection Frequency: 5 years

<u>Dock 26</u> Anticipated Remaining Useful Life: 2-5 years Preventative Maintenance Plan: Timber Curbing Repairs = \$45,600



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<u>Dock 28</u>

Anticipated Remaining Useful Life: 5-10 years Preventative Maintenance Plan: Pavement Repairs = \$ 18,200 Mooring Bollard Repairs = \$ 7,700 Timber Curbing Repairs = \$ 27,100 Bulkhead Sinkhole Fill = \$ 13,500 Capital Investments: Fender System Repairs = \$ 647,900 Inspection Frequency: 5 years



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Appendix A

Bathymetric Survey Image







Appendix B

Bulkhead Steel Thickness Measurements



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111 670761.056 2185400.592 0.825 0.87 0.892 0.748 112 670740.115 2185414.847 0.841 0.875 0.902 0.748 113 670719.722 218543.827 0.816 0.812 0.824 0.748 114 670699.247 218543.827 0.815 0.625 0.664 0.748 115 670679.137 2185457.841 0.82 0.812 0.896 0.748 116 670638.354 218545.257 0.795 0.767 0.794 0.748 117 670638.354 218550.579 0.899 0.792 0.782 0.748 119 670556.062 218551.257 0.797 0.788 0.866 0.748 120 670575.976 218552.939 0.802 0.776 0.814 0.748 121 67053.4731 218557.444 0.846 0.744 0.655 0.748 122 67043.456 2185571.26 0.798 0.652 0.636 <	110	670781.073	2185386.554	0.835	0.885	0.878	0.748
112 670740.115 2185414.847 0.841 0.875 0.902 0.748 113 670719.722 2185429.292 0.816 0.812 0.824 0.748 114 670699.247 218543.827 0.815 0.625 0.664 0.748 115 670679.137 218547.253 0.795 0.767 0.794 0.748 116 670658.113 2185472.563 0.795 0.767 0.794 0.748 117 670638.354 218549.579 0.809 0.792 0.782 0.748 118 670617.091 218550.579 0.809 0.792 0.782 0.748 120 670575.076 218551.557 0.797 0.788 0.866 0.748 121 670534.731 218553.449 0.768 0.666 0.656 0.748 122 670534.731 218557.126 0.798 0.616 0.636 0.748 123 670514.456 218557.126 0.755 0.664 0.748 </td <td>111</td> <td>670761.056</td> <td>2185400.592</td> <td>0.825</td> <td>0.87</td> <td>0.892</td> <td>0.748</td>	111	670761.056	2185400.592	0.825	0.87	0.892	0.748
113 670719.722 2185429.292 0.816 0.812 0.824 0.748 114 670699.247 218543.827 0.815 0.625 0.664 0.748 115 670679.137 2185457.841 0.82 0.812 0.896 0.748 116 670658.113 2185457.841 0.795 0.767 0.794 0.748 117 670638.354 2185455.414 0.798 0.792 0.782 0.748 118 670617.091 218550.579 0.809 0.792 0.782 0.748 119 67055.072 2185529.039 0.802 0.776 0.814 0.748 120 67055.077 218554.450 0.768 0.666 0.656 0.748 121 670514.56 218557.126 0.798 0.616 0.636 0.748 122 670514.456 218557.126 0.798 0.652 0.636 0.748 123 670472.919 2185602.058 0.655 0.648 0.748 <td>112</td> <td>670740.115</td> <td>2185414.847</td> <td>0.841</td> <td>0.875</td> <td>0.902</td> <td>0.748</td>	112	670740.115	2185414.847	0.841	0.875	0.902	0.748
114 670699.247 2185443.827 0.815 0.625 0.664 0.748 115 670679.137 2185457.841 0.82 0.812 0.896 0.748 116 670658.113 218547.841 0.795 0.767 0.794 0.748 117 670638.354 218545.441 0.798 0.792 0.782 0.748 118 670617.091 218550.579 0.809 0.792 0.782 0.748 120 670575.976 218552.57 0.797 0.788 0.866 0.748 121 67055.072 218557.444 0.846 0.704 0.665 0.748 122 670534.731 218557.449 0.846 0.666 0.665 0.748 123 670514.456 218557.126 0.798 0.616 0.632 0.748 124 670472.919 218560.099 0.793 0.652 0.634 0.748 125 670472.919 218560.268 0.799 0.632 0.72 <td< td=""><td>113</td><td>670719.722</td><td>2185429.292</td><td>0.816</td><td>0.812</td><td>0.824</td><td>0.748</td></td<>	113	670719.722	2185429.292	0.816	0.812	0.824	0.748
115 670679.137 2185457.841 0.82 0.812 0.896 0.748 116 670658.113 2185472.563 0.795 0.767 0.794 0.748 117 670638.354 2185485.414 0.798 0.792 0.782 0.748 118 670617.091 218550.579 0.809 0.792 0.782 0.748 119 670596.062 2185515.557 0.797 0.788 0.866 0.748 120 670575.976 2185543.469 0.768 0.666 0.656 0.748 121 670534.731 2185571.26 0.798 0.616 0.632 0.748 123 670514.456 2185571.26 0.798 0.616 0.632 0.748 124 67043.795 218558.132 0.825 0.666 0.632 0.748 125 670472.919 218560.099 0.733 0.652 0.636 0.748 126 67043.037 218562.58 0.799 0.632 0.722	114	670699.247	2185443.827	0.815	0.625	0.664	0.748
116 670658.113 2185472.563 0.795 0.767 0.794 0.748 117 670638.354 2185485.414 0.798 0.792 0.78 0.748 118 670617.091 218550.579 0.809 0.792 0.782 0.748 119 67055062 218551.257 0.777 0.814 0.748 120 67057.976 218552.9039 0.802 0.776 0.814 0.748 121 67055.097 218553.449 0.768 0.666 0.656 0.748 122 670514.456 218557.444 0.846 0.704 0.665 0.748 123 670514.456 218557.26 0.788 0.665 0.632 0.748 124 67043.793 218563.132 0.825 0.660 0.632 0.748 125 670472.919 218560.099 0.733 0.652 0.648 0.748 126 67041.442 218562.058 0.799 0.632 0.722 0.748	115	670679.137	2185457.841	0.82	0.812	0.896	0.748
117 670638.354 2185485.414 0.798 0.792 0.782 0.748 118 670617.091 2185500.579 0.809 0.792 0.782 0.748 119 670596.062 2185515.257 0.797 0.788 0.86 0.748 120 670575.076 2185529.039 0.802 0.766 0.814 0.748 121 67055.097 218553.469 0.768 0.666 0.656 0.748 122 670534.731 218557.444 0.846 0.704 0.665 0.748 123 670514.456 218557.1.26 0.798 0.616 0.636 0.748 124 67043.795 218560.099 0.793 0.652 0.636 0.748 125 67047.241 218562.587 0.835 0.655 0.648 0.748 126 670432.037 218562.587 0.835 0.616 0.688 0.748 127 670432.037 218562.587 0.815 0.663 0.644	116	670658.113	2185472.563	0.795	0.767	0.794	0.748
118 670617.091 2185500.579 0.809 0.792 0.782 0.748 119 670596.062 2185515.257 0.797 0.788 0.86 0.748 110 670596.062 2185515.257 0.797 0.788 0.86 0.748 120 670575.976 2185529.039 0.802 0.776 0.814 0.748 121 670554.731 218557.444 0.846 0.704 0.665 0.748 122 670514.456 2185571.26 0.798 0.616 0.636 0.748 123 670514.456 2185571.26 0.798 0.616 0.636 0.748 124 670439.75 218558.132 0.825 0.66 0.632 0.748 125 670472.919 218560.099 0.793 0.652 0.636 0.748 126 670454.72 218562.85 0.799 0.632 0.72 0.748 127 670432.037 2185642.404 0.825 0.616 0.688 <td< td=""><td>117</td><td>670638.354</td><td>2185485.414</td><td>0.798</td><td>0.792</td><td>0.78</td><td>0.748</td></td<>	117	670638.354	2185485.414	0.798	0.792	0.78	0.748
119 670596.062 2185515.257 0.797 0.788 0.86 0.748 120 670575.976 2185529.039 0.802 0.776 0.814 0.748 121 670575.976 218553.4469 0.768 0.666 0.656 0.748 122 67053.4731 218557.444 0.846 0.704 0.6655 0.748 123 670514.456 218557.126 0.798 0.616 0.636 0.748 124 670493.795 218558.132 0.825 0.66 0.632 0.748 125 670472.919 218560.099 0.793 0.652 0.636 0.748 126 670454.724 218562.858 0.799 0.632 0.72 0.748 127 670432.037 218562.858 0.799 0.632 0.644 0.748 128 670411.442 2185642.404 0.825 0.616 0.688 0.748 130 670390.787 218565.26 0.815 0.663 0.644	118	670617.091	2185500.579	0.809	0.792	0.782	0.748
120 670575.976 2185529.039 0.802 0.776 0.814 0.748 121 670555.097 2185543.469 0.768 0.66 0.656 0.748 122 670534.731 218557.444 0.846 0.704 0.665 0.748 123 670514.456 2185571.26 0.798 0.616 0.636 0.748 124 67043.755 2185571.26 0.793 0.652 0.636 0.748 125 670472.919 218560.099 0.733 0.652 0.636 0.748 126 670454.724 2185612.587 0.835 0.651 0.648 0.748 127 670432.037 218562.68 0.799 0.632 0.72 0.748 128 67041.442 218562.62 0.815 0.663 0.644 0.748 130 670369.945 2185670.763 0.798 0.684 0.628 0.748 131 670349.814 218568.48 0.789 0.672 0.642	119	670596.062	2185515.257	0.797	0.788	0.86	0.748
121 670555.097 2185543.469 0.768 0.66 0.656 0.748 122 670534.731 218557.444 0.846 0.704 0.665 0.748 123 670514.456 2185571.26 0.798 0.616 0.636 0.748 124 670493.795 218550.132 0.825 0.66 0.632 0.748 125 670472.191 218560.099 0.793 0.652 0.636 0.748 126 670454.724 2185602.099 0.793 0.652 0.648 0.748 127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 670411.442 2185642.404 0.825 0.616 0.688 0.748 130 670369.452 2185670.763 0.798 0.6632 0.644 0.748 131 670349.814 218564.48 0.789 0.672 0.642 0.748 132 670349.814 2185648.48 0.789 0.628 0.642	120	670575.976	2185529.039	0.802	0.776	0.814	0.748
122 670534.731 2185557.444 0.846 0.704 0.665 0.748 123 670514.456 2185571.26 0.798 0.616 0.636 0.748 124 670493.795 2185585.132 0.825 0.666 0.632 0.748 125 670472.919 218560.099 0.793 0.652 0.636 0.748 126 670454.724 2185612.587 0.835 0.655 0.648 0.748 127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 670411.442 218562.62 0.815 0.663 0.644 0.748 129 670390.787 218564.84 0.789 0.632 0.72 0.748 130 670369.945 2185670.763 0.798 0.684 0.628 0.748 131 67034.814 218564.48 0.789 0.624 0.748 132 67038.805 218579.729 0.801 0.684 0.644 0.748	121	670555.097	2185543.469	0.768	0.66	0.656	0.748
123 670514.456 2185571.26 0.798 0.616 0.636 0.748 124 670493.795 2185585.132 0.825 0.66 0.632 0.748 125 670472.919 218560.099 0.793 0.652 0.636 0.748 126 67047.2919 2185602.099 0.793 0.652 0.636 0.748 126 670454.724 2185612.587 0.835 0.655 0.648 0.748 127 670432.037 218562.8058 0.799 0.632 0.72 0.748 128 670411.442 218564.2404 0.825 0.616 0.688 0.748 129 670390.787 218567.763 0.798 0.684 0.628 0.748 130 670349.814 218568.514 0.810 0.622 0.624 0.748 131 670349.814 218569.8514 0.811 0.623 0.624 0.748 132 67038.199 2185712.793 0.801 0.628 0.644	122	670534.731	2185557.444	0.846	0.704	0.665	0.748
124 670493.795 2185585.132 0.825 0.66 0.632 0.748 125 670472.919 2185600.099 0.793 0.652 0.636 0.748 126 670454.724 2185612.587 0.835 0.652 0.632 0.748 127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 670411.442 2185642.404 0.825 0.616 0.688 0.748 129 670390.787 2185562.66 0.815 0.663 0.644 0.748 130 670369.945 2185670.753 0.798 0.684 0.628 0.748 131 670349.814 218568.548 0.789 0.624 0.748 132 670328.05 2185712.793 0.801 0.688 0.644 0.748 133 67038.199 218572.7294 0.798 0.628 0.644 0.748 134 670287.701 218572.529 0.821 0.638 0.644 0.748 <	123	670514.456	2185571.26	0.798	0.616	0.636	0.748
125 670472.919 2185600.099 0.793 0.652 0.636 0.748 126 670454.724 2185612.587 0.835 0.65 0.648 0.748 127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 670411.442 218562.058 0.799 0.632 0.72 0.748 128 670411.442 218562.66 0.815 0.663 0.644 0.748 130 67039.787 2185652.66 0.815 0.663 0.644 0.748 131 670349.814 2185684.48 0.789 0.672 0.642 0.748 132 670328.05 2185691.743 0.811 0.632 0.624 0.748 133 670308.199 218572.793 0.801 0.684 0.748 134 670267.371 2185749.333 0.857 0.628 0.644 0.748 135 670246.623 2185755.892 0.818 0.644 0.748 1	124	670493.795	2185585.132	0.825	0.66	0.632	0.748
126 670454.724 2185612.587 0.835 0.65 0.648 0.748 127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 67041.442 2185642.404 0.825 0.616 0.688 0.748 129 670390.787 218565.26 0.815 0.663 0.644 0.748 130 670369.454 218567.0763 0.798 0.628 0.748 131 670349.814 2185694.48 0.789 0.628 0.748 132 670328.805 2185698.514 0.811 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670267.701 218572.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 218575.892 0.818 0.624 0.748 137 6	125	670472.919	2185600.099	0.793	0.652	0.636	0.748
127 670432.037 2185628.058 0.799 0.632 0.72 0.748 128 670411.442 2185642.404 0.825 0.616 0.688 0.748 129 670390.787 2185656.26 0.815 0.663 0.644 0.748 130 670369.945 2185670.763 0.798 0.663 0.642 0.748 131 670349.814 2185684.48 0.789 0.672 0.642 0.748 132 670328.805 2185698.514 0.81 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670267.701 218572.724 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 218575.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.676 0.748 <	126	670454.724	2185612.587	0.835	0.65	0.648	0.748
128 670411.442 2185642.404 0.825 0.616 0.688 0.748 129 670390.787 2185656.26 0.815 0.663 0.644 0.748 130 670369.945 2185670.763 0.798 0.684 0.628 0.748 131 670349.814 218568.48 0.789 0.672 0.624 0.748 132 670328.805 2185698.514 0.81 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670287.701 218572.7294 0.798 0.628 0.644 0.748 135 670267.71 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 218575.892 0.818 0.644 0.748 137 670226.633 2185769.554 0.818 0.644 0.748 137 670226.633 2185769.554 0.818 0.766 0.748 138 <td< td=""><td>127</td><td>670432.037</td><td>2185628.058</td><td>0.799</td><td>0.632</td><td>0.72</td><td>0.748</td></td<>	127	670432.037	2185628.058	0.799	0.632	0.72	0.748
129 670390.787 2185656.26 0.815 0.663 0.644 0.748 130 670369.945 2185670.763 0.798 0.684 0.628 0.748 131 670349.814 218568.448 0.789 0.672 0.642 0.748 132 670328.05 2185698.514 0.81 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.688 0.684 0.748 134 670287.701 218572.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.393 0.857 0.628 0.644 0.748 136 670246.628 2185755.892 0.818 0.624 0.748 137 670226.633 218579.554 0.818 0.766 0.748 137 670226.633 218579.554 0.818 0.766 0.748 138 670205.429 218578.4241 0.823 0.788 0.782 0.748	128	670411.442	2185642.404	0.825	0.616	0.688	0.748
130 670369.945 2185670.763 0.798 0.684 0.628 0.748 131 670349.814 2185684.48 0.789 0.672 0.642 0.748 132 670328.805 2185698.514 0.81 0.632 0.624 0.748 133 67038.199 2185712.793 0.801 0.68 0.684 0.748 134 67028.701 2185727.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.644 0.748 136 670264.628 218575.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 218578.4241 0.823 0.788 0.782 0.748	129	670390.787	2185656.26	0.815	0.663	0.644	0.748
131 670349.814 2185684.48 0.789 0.672 0.642 0.748 132 670328.805 2185698.514 0.81 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670287.701 2185727.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670267.371 218575.892 0.821 0.638 0.644 0.748 136 670264.628 2185755.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 218578.4241 0.823 0.788 0.782 0.748	130	670369.945	2185670.763	0.798	0.684	0.628	0.748
132 670328.805 2185698.514 0.81 0.632 0.624 0.748 133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670287.701 2185727.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 218575.892 0.821 0.638 0.644 0.748 137 670226.633 218579.554 0.818 0.76 0.796 0.748 138 670205.429 218578.4241 0.823 0.788 0.782 0.748	131	670349.814	2185684.48	0.789	0.672	0.642	0.748
133 670308.199 2185712.793 0.801 0.68 0.684 0.748 134 670287.701 2185727.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 218575.892 0.812 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 2185784.241 0.823 0.788 0.782 0.748	132	670328.805	2185698.514	0.81	0.632	0.624	0.748
134 670287.701 2185727.294 0.798 0.628 0.644 0.748 135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 2185755.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.766 0.796 0.748 138 670205.429 2185784.241 0.823 0.788 0.782 0.748	133	670308.199	2185712.793	0.801	0.68	0.684	0.748
135 670267.371 2185740.933 0.857 0.628 0.672 0.748 136 670246.628 2185755.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 2185784.241 0.823 0.788 0.782 0.748	134	670287.701	2185727.294	0.798	0.628	0.644	0.748
136 670246.628 2185755.892 0.821 0.638 0.644 0.748 137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 2185784.241 0.823 0.788 0.782 0.748	135	670267.371	2185740.933	0.857	0.628	0.672	0.748
137 670226.633 2185769.554 0.818 0.76 0.796 0.748 138 670205.429 2185784.241 0.823 0.788 0.782 0.748	136	670246.628	2185755.892	0.821	0.638	0.644	0.748
138 670205.429 2185784.241 0.823 0.788 0.782 0.748	137	670226.633	2185769.554	0.818	0.76	0.796	0.748
	138	670205.429	2185784.241	0.823	0.788	0.782	0.748
139 670186.189 2185798.152 0.809 0.792 0.76 0.748	139	670186.189	2185798.152	0.809	0.792	0.76	0.748
140 670164.662 2185812.748 0.799 0.58 0.844 0.748	140	670164.662	2185812.748	0.799	0.58	0.844	0.748
141 670144.109 2185827.092 0.798 0.74 0.44 0.748	141	670144.109	2185827.092	0.798	0.74	0.44	0.748



(*) - Ultrasonic measurements may be greater than original wall thickness due to location of reading. If location of reading is near corner or joint it will be greater than the wall thickness

SOUTH BULKHEAD BETWEEN DOCK 22 AND DOCK 24						
Survey Boint	Lat	Long	Wa	all thickness	(in)	Original Wall Thickness (*)
Survey Fornt	North	East	Тор	Middle	Bottom	(in.)
142	670152.468	2185845.926	0.799	0.536	0.672	0.5
143	670166.865	2185866.367	0.768	0.668	0.744	0.5
144	670181.344	2185887.49	0.485	0.496	0.52	0.5
145	670195.462	2185907.49	0.531	0.484	0.76	0.5
146	670209.661	2185928.283	0.512	0.516	0.56	0.5
147	670223.67	2185948.951	0.537	0.58	0.524	0.5
148	670237.304	2185969.804	0.469	0.412	0.472	0.5
149	670251.271	2185990.168	0.437	0.78	0.58	0.5
150	670265.512	2186011.065	0.485	0.58	0.356	0.5
P	-					
			DOCK 24	WEST		
Survey Deint	Lat	Long	Wa	all thickness	(in)	Original Wall Thickness (*)
Survey Fornt	North	East	Тор	Middle	Bottom	(in.)
151	670281.105	2186020.667	0.679	0.578	0.612	0.5
152	670301.939	2186006.365	0.699	0.528	0.532	0.5
153	670322.529	2185992.081	0.676	0.624	0.584	0.5
154	670343.215	2185977.92	0.704	0.578	0.408	0.5
155	670363.392	2185963.709	0.619	0.486	0.464	0.5
156	670384.089	2185949.267	0.645	0.448	0.388	0.5
157	670404.561	2185935.529	0.668	0.44	0.76	0.5
158	670425.01	2185921.156	0.645	0.412	0.392	0.5
159	670445.305	2185907.278	0.725	0.502	0.519	0.5
160	670466.112	2185892.378	0.658	0.538	0.502	0.5
161	670487.17	2185878.853	0.644	0.528	0.522	0.5
162	670507.68	2185864.545	0.668	0.538	0.512	0.5
163	670528.312	2185850.376	0.652	0.502	0.472	0.5
164	670548.808	2185835.981	0.646	0.58	0.511	0.5
165	670569.646	2185821.602	0.647	0.47	0.48	0.5
166	670590.033	2185807.67	0.651	0.506	0.551	0.5
167	670610.268	2185793.851	0.598	0.512	0.508	0.5
168	670631.731	2185778.893	0.627	0.506	0.504	0.5
169	670652.128	2185765.03	0.654	0.505	0.51	0.5
170	670672.187	2185751.179	0.65	0.501	0.506	0.5
171	670693.074	2185736.728	0.649	0.509	0.507	0.5
172	670713.844	2185722.131	0.529	0.491	0.426	0.5
173	670734.076	2185708.202	0.66	0.52	0.485	0.5
174	670755.965	2185693.545	0.608	0.501	0.487	0.5
175	670775.814	2185679.591	0.603	0.728	0.717	0.5
176	670796.289	2185665.19	0.647	0.708	0.71	0.5
177	670816.907	2185651.089	0.636	0.768	0.763	0.5
178	670836.388	2185637.132	0.64	0.749	0.758	0.5
179	670858.661	2185623.335	0.613	0.645	0.551	0.5



(*) - Ultrasonic measurements may be greater than original wall thickness due to location of reading. If location of reading is near corner or joint it will be greater than the wall thickness

DOCK 24 NORTH						
Survey Deint	Lat	Long	Wa	III thickness	(in)	Original Wall Thickness (*)
Survey Fornt	North	East	Тор	Middle	Bottom	(in.)
180	670877.985	2185632.985	0.677	0.751	0.704	0.5
181	670893.488	2185653.274	0.627	0.708	0.754	0.5
182	670908.237	2185672.882	0.63	0.695	0.744	0.5
183	670923.639	2185692.826	0.632	0.763	0.768	0.5
184	670938.97	2185712.414	0.645	0.708	0.761	0.5
185	670953.894	2185731.946	0.654	0.72	0.724	0.5
186	670969.39	2185751.837	0.623	0.705	0.702	0.5
187	670984.409	2185771.394	0.63	0.671	0.632	0.5
188	670999.838	2185791.328	0.628	0.721	0.696	0.5
189	671015.313	2185810.989	0.632	0.712	0.71	0.5
190	671030.719	2185830.655	0.585	0.697	0.705	0.5
191	671045.886	2185850.214	0.636	0.574	0.683	0.5
192	671061.492	2185870.079	0.625	0.53	0.531	0.5
193	671077.124	2185889.602	0.691	0.595	0.55	0.5
194	671092.604	2185909.723	0.672	0.686	0.656	0.5
195	671107.936	2185929.025	0.615	0.517	0.619	0.5
196	671123.335	2185948.751	0.605	0.554	0.568	0.5
197	671138.506	2185968.559	0.628	0.639	0.712	0.5
198	671153.586	2185988.304	0.66	0.654	0.628	0.5
199	671169.089	2186008.064	0.603	0.611	0.701	0.5
200	671178.587	2186030.493	614	0.579	0.576	0.5

DOCK 24 EAST						
Survey Boint	Lat	Long	Wa	III thickness	(in)	Original Wall Thickness (*)
Survey Fornt	North	East	Тор	Middle	Bottom	(in.)
204	671159.697	2186047.02	0.623	0.64	0.68	0.5
205	671138.11	2186060.59	0.661	0.702	0.78	0.5
206	671116.074	2186075.26	0.66	0.71	0.725	0.5
207	671097.54	2186088.107	0.675	0.715	0.812	0.5
208	671076.087	2186102.718	0.714	0.688	0.602	0.5
209	671054.648	2186117.213	0.698	0.704	1.048	0.5
210	671033.904	2186131.637	0.736	0.668	0.788	0.5
211	671012.924	2186145.23	0.758	0.698	1.02	0.5
212	670993.393	2186159.025	0.718	0.703	0.98	0.5
213	670972.641	2186173.034	0.738	0.663	1.01	0.5
214	670951.601	2186187.195	0.725	0.784	1.04	0.5
215	670932.069	2186201.127	0.687	0.802	0.785	0.5
216	670909.764	2186217.004	0.71	0.89	1.015	0.5
217	670890.19	2186230.559	0.805	0.705	1.002	0.5
218	670869.795	2186244.243	0.79	0.802	1.034	0.5
219	670849.834	2186258.566	0.708	0.738	0.987	0.5
220	670828.855	2186272.963	0.879	0.703	1.023	0.5
221	670808.619	2186286.718	0.79	0.795	1.019	0.5
222	670787.891	2186301.129	0.715	0.668	1.015	0.5
223	670767	2186315.231	0.708	0.72	1.013	0.5
224	670747.203	2186328.892	0.609	0.701	1.021	0.5
225	670726.119	2186342.75	0.705	0.724	0.75	0.5
226	670705.058	2186357.061	0.68	0.694	0.675	0.5
227	670684.991	2186371.233	0.636	0.702	0.689	0.5
228	670664.67	2186385.751	0.61	0.628	0.769	0.5
229	670644.821	2186398.662	0.667	0.479	0.505	0.5



(*) - Ultrasonic measurements may be greater than original wall thickness due to location of reading. If location of reading is near corner or joint it will be greater than the wall thickness

SOUTH BULKHEAD BETWEEN DOCK 24 AND DOCK 26											
Survey Reint	Lat	Long	Wa	III thickness	(in)	Original Wall Thickness (*)					
Survey Fornt	North	East	Тор	Middle Bottom		(in.)					
230	670635.098	2186418.15	0.589	0.485 0.477		0.5					
231	670646.582	2186434.631	0.54	0.49	0.46	0.5					
232	670660.926	2186455.847	0.55	0.517	0.56	0.5					
233	670675.212	2186476.036	0.58	0.506 0.521		0.5					
234	670689.003	2186496.992	0.59	0.493	0.49	0.5					
235	670703.398	2186517.699	0.556	0.535	0.505	0.5					
236	670717.838	2186538.505	0.568	0.512	0.516	0.5					
237	670731.758	2186558.827	0.598	0.51	0.518	0.5					
238 670745.944 2186579.74 0.575 0.508 0.502 0.5											
DOCK 26 NORTH											

Survey Point	Lat	Long	Wa	II thickness	(in)	Original Wall Thickness (*)	
	North	East	Тор	Middle	Bottom	(in.)	
266	671318.04	2186211.218	0.601	0.52	0.525	0.5	
267	671332.797	2186229.871	0.625	0.54	0.548	0.5	
268	671348.055	2186249.741	0.657	0.577	0.526	0.5	
269	671362.548	2186269.336	6269.336 0.638 0		0.548	0.5	
270	671378.189	2186288.377	0.645	0.58	0.538	0.5	
271	671392.842	2186308.789	0.648	0.52	0.53	0.5	
272	671408.277	2186328.715	0.653	0.552	0.531	0.5	
273	671424.829	2186349.528	0.625	0.566	0.535	0.5	
274	671440.185	2186369.369	0.634	534 0.532 0.534		0.5	
275	671455.114	2186389.159	0.621	0.561	0.542	0.5	
276	671470.314	2186407.843	0.619	0.553	0.536	0.5	
277	671486.514	2186428.975	0.642	0.554	0.573	0.5	

DOCK 26 EAST											
Survey Deint	Lat	Long	Wa	all thickness	(in)	Original Wall Thickness (*)					
Survey Point	North	East	Тор	Middle	Bottom	(in.)					
278	671489.423	2186446.91	0.576	0.566	0.553	0.5					
279	671467.502	2186461.587	0.562	0.57	0.576	0.5					
282	671447.95	2186475.069	0.548	0.568	0.524	0.5					
283	671426.826	2186489.957	0.580	0.588	0.592	0.5					
284	671406.177	2186503.664	0.558	0.525	0.572	0.5					
285	671385.396	2186517.626	0.548	0.588	0.540	0.5					
286	671366.063	2186530.88	0.564	0.528	0.598	0.5					
287	671345.011	2186545.231	0.584	0.501	0.580	0.5					
288	671323.668	2186559.373	0.560	0.540	0.536	0.5					
289	671303.3	71303.3 2186574.025		0.545	0.520	0.5					
290	671282.527	2186588.202	0	0.576	0.495	0.5					
291	671261.894	2186601.808	0.556	0.520	0.564	0.5					
292	671242.468	2186615.549	0.584	0.520	0.530	0.5					
293	671220.055	2186631.069	0.564	0.584	0.596	0.5					
294	671200.483	2186644.157	0.560	0.656	0.548	0.5					
295	671178.86	2186659.26	0.580	0.552	0.558	0.5					
296	671159.408	2186672.452	0.550	0.540	0.634	0.5					
297	671136.621	2186688.364	0.562	0.598	0.568	0.5					
298	671118.31	2186700.654	0.548	0.576	0.538	0.5					
299	671098.504	2186714.012	0.680	0.660	0.710	0.5					
300	671077.464	2186728.423	0.572	0.648	0.701	0.5					
301	671056.901	2186742.387	0.680	0.617	0.650	0.5					
302	671035.991	2186757.047	0.660	0.680	0.690	0.5					
303	671014.611	2186771.52	0.684	0.632	0.685	0.5					
304	670993.835	2186785.585	0.687	0.662	0.725	0.5					
305	670973.58	2186800.5	0.722	0.711	0.702	0.5					
306	670952.669	2186813.667	0.552	0.660	0.952	0.5					
307	670931.788	2186827.868	0.544	0.496	0.600	0.5					



(*) - Ultrasonic measurements may be greater than original wall thickness due to location of reading. If location of reading is near corner or joint it will be greater than the wall thickness

SOUTH BULKHEAD BETWEEN DOCK 26 AND DOCK 28										
C. mure Delint	Lat	Long	(in)	Original Wall Thickness (*)						
Survey Point	North	East	Тор	Middle	Bottom	(in.)				
308	670928.554	2186844.634	0.700	0.544	0.584	0.5				
309	670942.324	2186864.807	0.548	0.55	0.528	0.5				
310	670956.266	2186885.169	0.55	0.493	0.501	0.5				
311	670970.476	2186906.112	0.495	0.568	0.536	0.5				
312	670984.602	2186927.52	0.495	0.501	0.497	0.5				
313	670998.538	2186947.973	0.530	0.512	0.598	0.5				
314	671013.056	2186968.658	0.510	0.522	0.515	0.5				
315	671027.434	2186989.093	0.570	0.501	0.489	0.5				
316	671040.804	2187009.926	0.595	0.560	0.490	0.5				
			DOCK 28	WEST						
Survey Point	Lat	Long	Wa	II thickness	(in)	Original Wall Thickness (*)				
Survey Form	North	East	Тор	Middle	Bottom	(in.)				
317	671056.305	2187020.913	0.501	0.540	0.525	0.5				
318	671076.21	2187007.045	0.540	0.510	0.492	0.5				
319	671096.833	2186992.265	0.504	0.550	0.515	0.5				
320	671118.067	2186978.044	0.531	0.501	0.528	0.5				
321	671138.785	2186964.08	0.520	0.536	0.500	0.5				
322	671158.645	2186950.814	0.538	0.504	0.498	0.5				
323	671179.913	2186935.851	0.505	0.538	0.501	0.5				
324	671200.507	2186922.217	0.535	0.568	0.488	0.5				
325	671221.644	2186907.457	0.510	0.520	0.489	0.5				
326	671241.818	2186893.367	0.499	0.528	0.505	0.5				
327	671263.013	2186879.639	0.528	0.530	0.488	0.5				
328	671284.016	2186864.598	0.565	0.454	0.408	0.5				
329	671303.649	2186851.291	0.632	0.542	0.428	0.5				
330	671324.963	2186836.544	0.545	0.492	0.450	0.5				
331	671345.075	2186822.794	0.502	0.524	0.468	0.5				
332	671365.464	2186809.361	0.498	0.476	0.456	0.5				
333	671386.174	2186794.645	0.505	0.498	0.432	0.5				
334	671406.567	2186780.522	0.470	0.468	0.520	0.5				
335	671426.776	2186766.414	0.548	0.488	0.508	0.5				
336	671447.299	2186752.55	0.564	0.504	0.524	0.5				
337	671468.502	2186738.136	0.490	0.528	0.510	0.5				
338	671489.294	2186723.52	0.540	0.489	0.496	0.5				
339	671509.118	2186709.236	0.532	0.496	0.482	0.5				
340	671530.12	2186695.312	0.520	0.515	0.490	0.5				
341	671551.279	2186681.386	0.528	0.492	0.418	0.5				



(*) - Ultrasonic measurements may be greater than original wall thickness due to location of reading. If location of reading is near corner or joint it will be greater than the wall thickness

DOCK 28 NORTH										
Survey Point	Lat	Long	Wa	Original Wall Thickness (*)						
	North	East	East Top		Bottom	(in.)				
345	671633.334	2186624.871	0.552	0.492	0.425	0.5				
346	671650.182	2186640.475	0.489	0.488	0.497	0.5				
347	671663.833	2186658.986	0.540	0.484	0.450	0.5				
348	671680.055	2186679.646	0.492	0.577	0.489	0.5				
349	671694.94	2186699.518	0.552	0.548	0.515	0.5				

0.510

0.495

671572.397 2186667.312

2186653.434

671592.761

0.480

0.496

0.455

0.435

0.5

0.5

342

343



Appendix C

Construction Cost Estimates



		ESTIMATED MAINTENANCE AND REPAIR COSTS												
		Construction										Inspection	Contigency	Total
Dock 22	Mobilization	Timber	Pavement	Fender	Conc Cap	Sheeting	Bollard	Office	Supervision	Sub-Total	Sub-Total	Sub-Total	Sub-Total	
Short Term	\$2,000	\$7,400	\$15,500		\$19,800		\$5,500		\$5,000	\$55,200	\$8,000	\$5,000	\$13,640	\$82,100
Long Term	\$4,000			\$25,300					\$10,000	\$39,300	\$25,000	\$15,000	\$15,860	\$95,200
Dock 24														
Short Term	\$4,000	\$5,500					\$38,600		\$5,000	\$53,100	\$23,500	\$19,000	\$19,120	\$114,900
Long Term	\$40,000			\$138,900	\$759,600			\$10,000	\$40,000	\$988,500	\$45,000	\$38,000	\$214,300	\$1,285,900
Dock 26														
Short Term	\$4,000	\$18,100	\$10,400				\$18,500		\$5,000	\$56,000	\$23,500	\$19,000	\$19,700	\$118,400
Long Term	\$100,000			\$414,400		\$2,750,000		\$20,000	\$80,000	\$3,364,400	\$10,000	\$6,000	\$676,080	\$4,056,600
											l			1
Dock 28														1
Short Term	\$2,000	\$15,500	\$10,400			\$6,700	\$4,400		\$5,000	\$44,000	\$10,000	\$8,000	\$12,400	\$66,500
Long Term	\$20,000			\$281,400				\$7,500	\$20,000	\$328,900	\$115,000	\$96,000	\$107,980	\$647,900